

M-OSRP

Mission - Oriented Seismic Research Program
Solve The Right Problem



Direct Inversion and FWI A key-note address

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Society of Exploration Geophysicists
The international society of applied geophysics

SEG WORKSHOP

Full-waveform Inversion: Filling the Gaps

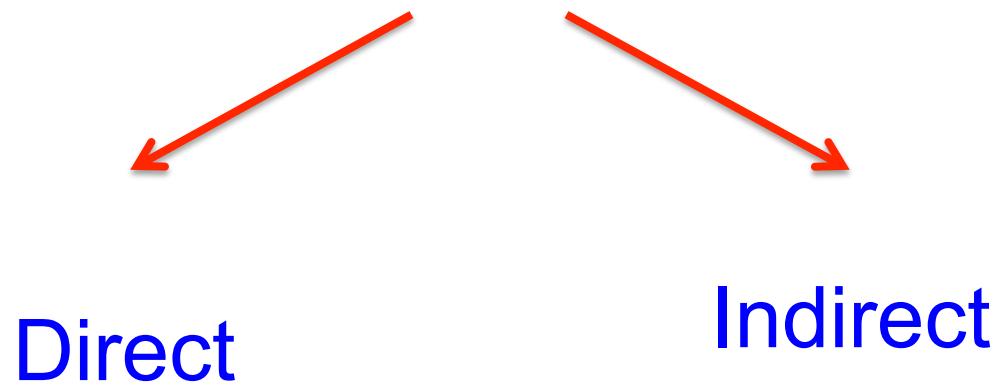
30 March–1 April 2015
Abu Dhabi, UAE



SEG Middle East
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- Modeling
- Inversion



Direct

$$ax^2 + bx + c = 0$$

$$x = \frac{-b \pm \sqrt{b^2 - 4ac}}{2a}$$

Indirect

Search for x such that

$(ax^2 + bx + c)^2$ is a minimum

Indicators of “indirect”

- model matching
- objective/cost functions
- search algorithm
- iterative linear “inversion”
- necessary and not sufficient conditions, e.g., CIG
flatness

There's a role for direct and indirect methods in practical real world application.

Direct Forward and Direct Inverse

$$L_0 G_0 = \delta \quad LG = \delta$$

$$V = L_0 - L \quad \psi_s = G - G_0$$

Relationship $G = G_0 + G_0 V G \quad (1)$

An operator identity that follows from

$$L^{-1} = L_0^{-1} + L_0^{-1} (L_0 - L) L^{-1}$$

Modeling $L \rightarrow G \quad L_0, V \rightarrow G$

Direct Forward and Direct Inverse

Relationship

$$G = G_0 + G_0 V G \quad (1)$$

Modeling

$$G = G_0 + G_0 V G_0 + G_0 V G_0 V G_0 + \dots \quad (2)$$

Form

$$G - G_0 = S = ar + ar^2 + \dots = \frac{ar}{1 - r}$$

with

$$a = G_0$$

$$r = V G_0$$

$$S = S_1 + S_2 + S_3 + \dots$$

Direct Forward and Direct Inverse

$$S = S_1 + S_2 + S_3 + \dots$$

$$S = \frac{ar}{1-r}$$

Solve for r

$$\begin{aligned} r &= \frac{S/a}{1 + S/a} = S/a - \left(S/a\right)^2 + \left(S/a\right)^3 + \dots \\ &= r_1 + r_2 + r_3 + \dots \end{aligned}$$

Direct Forward and Direct Inverse

$$S = (G - G_0)_{ms} = Data$$

Forward S in terms of V , inverse V in terms of S

$$V = V_1 + V_2 + \cdots \quad (3)$$

where V_n is the portion of V , n-th order in the data

(2) is the forward series;

(3) is the inverse series.

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- The relationship (2) provides a Geometric forward series rather than a Taylor series.
 - In general, a Taylor series doesn't have an inverse series; however, a Geometric series has an inverse series.
 - All conventional current mainstream inversion, including iterative linear inversion and FWI, are based on a Taylor series concept.
 - Solving a forward problem in an inverse sense is not the same as solving an inverse problem directly.

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- The r_1, r_2, \dots equations generalize

$$\begin{aligned} r &= S/a - \left(S/a\right)^2 + \left(S/a\right)^3 + \dots \\ &= r_1 + r_2 + r_3 + \dots \end{aligned}$$

$$G_0 V_1 G_0 = D$$

$$G_0 V_2 G_0 = -G_0 V_1 G_0 V_1 G_0$$

$$G_0 V_3 G_0 = -G_0 V_1 G_0 V_1 G_0 V_1 G_0 + \dots$$

(2D) Elastic (isotropic)

$$L\vec{u} = \begin{pmatrix} f_x \\ f_z \end{pmatrix} \quad \hat{L} \begin{pmatrix} \phi^P \\ \phi^S \end{pmatrix} = \begin{pmatrix} F^P \\ F^S \end{pmatrix}$$

where

$$L = \left[\rho \omega^2 \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix} + \begin{pmatrix} \partial_x \gamma \partial_x + \partial_z \mu \partial_z & \partial_x (\gamma - 2\mu) \partial_z + \partial_z \mu \partial_x \\ \partial_z (\gamma - 2\mu) \partial_x + \partial_x \mu \partial_z & \partial_z \gamma \partial_z + \partial_x \mu \partial_x \end{pmatrix} \right]$$

$$L_0 = \left[\rho_0 \omega^2 \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix} + \begin{pmatrix} \gamma_0 \partial_x^2 + \mu_0 \partial_z^2 & (\gamma_0 - \mu_0) \partial_x \partial_z \\ (\gamma_0 - \mu_0) \partial_x \partial_z & \mu_0 \partial_x^2 + \gamma_0 \partial_z^2 \end{pmatrix} \right]$$

$$V \equiv L_0 - L$$

$$= \begin{bmatrix} a_\rho \omega^2 + \alpha_0^2 \partial_x a_\gamma \partial_x + \beta_0^2 \partial_z a_\mu \partial_z & \partial_x (\alpha_0^2 a_\gamma - 2\beta_0^2 a_\mu) \partial_z + \beta_0^2 \partial_z a_\mu \partial_x \\ \partial_z (\alpha_0^2 a_\gamma - 2\beta_0^2 a_\mu) \partial_x + \beta_0^2 \partial_x a_\mu \partial_z & a_\rho \omega^2 + \alpha_0^2 \partial_z a_\gamma \partial_z + \beta_0^2 \partial_x a_\mu \partial_x \end{bmatrix}$$

$$a_\rho \equiv \frac{\rho}{\rho_0} - 1, a_\gamma \equiv \frac{\gamma}{\gamma_0} - 1, a_\mu \equiv \frac{\mu}{\mu_0} - 1$$

The forward problem

$$\hat{G} - \hat{G}_0 = \hat{G}_0 \hat{V} \hat{G} = \hat{G}_0 \hat{V} \hat{G}_0 + \hat{G}_0 \hat{V} \hat{G}_0 \hat{V} \hat{G}_0 + \dots \quad (4)$$

$$\begin{aligned} \begin{pmatrix} \hat{D}^{PP} & \hat{D}^{PS} \\ \hat{D}^{SP} & \hat{D}^{SS} \end{pmatrix} &= \begin{pmatrix} \hat{G}_0^P & 0 \\ 0 & \hat{G}_0^S \end{pmatrix} \begin{pmatrix} \hat{V}^{PP} & \hat{V}^{PS} \\ \hat{V}^{SP} & \hat{V}^{SS} \end{pmatrix} \begin{pmatrix} \hat{G}_0^P & 0 \\ 0 & \hat{G}_0^S \end{pmatrix} \\ &+ \begin{pmatrix} \hat{G}_0^P & 0 \\ 0 & \hat{G}_0^S \end{pmatrix} \begin{pmatrix} \hat{V}^{PP} & \hat{V}^{PS} \\ \hat{V}^{SP} & \hat{V}^{SS} \end{pmatrix} \begin{pmatrix} \hat{G}_0^P & 0 \\ 0 & \hat{G}_0^S \end{pmatrix} \\ &\begin{pmatrix} \hat{V}^{PP} & \hat{V}^{PS} \\ \hat{V}^{SP} & \hat{V}^{SS} \end{pmatrix} \begin{pmatrix} \hat{G}_0^P & 0 \\ 0 & \hat{G}_0^S \end{pmatrix} \\ &+ \dots \end{aligned}$$

The inverse problem (solving for r in terms of S)

$$\begin{aligned}\hat{V}^{PP} &= \hat{V}_1^{PP} + \hat{V}_2^{PP} + \hat{V}_3^{PP} + \dots \\ \hat{V}^{PS} &= \hat{V}_1^{PS} + \hat{V}_2^{PS} + \hat{V}_3^{PS} + \dots \\ \hat{V}^{SP} &= \hat{V}_1^{SP} + \hat{V}_2^{SP} + \hat{V}_3^{SP} + \dots \\ \hat{V}^{SS} &= \hat{V}_1^{SS} + \hat{V}_2^{SS} + \hat{V}_3^{SS} + \dots\end{aligned}\tag{5}$$

$$\hat{V}^{PP} = -\nabla^2 a_\gamma - \frac{\omega^2}{\alpha_0^2} (a_\rho \partial_x^2 + \partial_z a_\rho \partial_z) \frac{1}{\nabla^2} - \left[-2\partial_z^2 a_{mu} \partial_x^2 - 2\partial_x^2 a_{mu} \partial_z^2 + 4\partial_x^2 \partial_z a_{mu} \partial_z \right] \frac{1}{\nabla^2}$$

$$\hat{V}^{PS} = \frac{\alpha_0^2}{\beta_0^2} \left[\frac{\omega^2}{\alpha_0^2} (\partial_x a_\rho \partial_z - \partial_z a_\rho \partial_x) + 2\partial_x \partial_z a_{mu} (\partial_z^2 - \partial_x^2) - 2(\partial_z^2 - \partial_x^2) a_{mu} \partial_z \partial_x \right] \frac{1}{\nabla^2}$$

$$\hat{V}^{SP} = - \left[\frac{\omega^2}{\alpha_0^2} (\partial_x a_\rho \partial_z - \partial_z a_\rho \partial_x) + 2\partial_x \partial_z a_{mu} (\partial_z^2 - \partial_x^2) - 2(\partial_z^2 - \partial_x^2) a_{mu} \partial_z \partial_x \right] \frac{1}{\nabla^2}$$

$$\hat{V}^{SS} = - \frac{\alpha_0^2}{\beta_0^2} \left[\frac{\omega^2}{\alpha_0^2} (a_\rho \partial_x^2 + \partial_z a_\rho \partial_z) + (\partial_z^2 - \partial_x^2) a_{mu} (\partial_z^2 - \partial_x^2) + 4\partial_x \partial_z a_{mu} \partial_x \partial_z \right] \frac{1}{\nabla^2}$$

$$a_{mu} = \frac{\mu - \mu_0}{\gamma_0} = \frac{\beta_0^2}{\alpha_0^2} a_\mu$$

$$\begin{pmatrix} \hat{D}^{PP} & \hat{D}^{PS} \\ \hat{D}^{SP} & \hat{D}^{SS} \end{pmatrix} = \begin{pmatrix} \hat{G}_0^P & 0 \\ 0 & \hat{G}_0^S \end{pmatrix} \begin{pmatrix} \hat{V}_1^{PP} & \hat{V}_1^{PS} \\ \hat{V}_1^{SP} & \hat{V}_1^{SS} \end{pmatrix} \begin{pmatrix} \hat{G}_0^P & 0 \\ 0 & \hat{G}_0^S \end{pmatrix} \quad (6)$$

$$\begin{aligned} & \begin{pmatrix} \hat{G}_0^P & 0 \\ 0 & \hat{G}_0^S \end{pmatrix} \begin{pmatrix} \hat{V}_2^{PP} & \hat{V}_2^{PS} \\ \hat{V}_2^{SP} & \hat{V}_2^{SS} \end{pmatrix} \begin{pmatrix} \hat{G}_0^P & 0 \\ 0 & \hat{G}_0^S \end{pmatrix} \\ &= - \begin{pmatrix} \hat{G}_0^P & 0 \\ 0 & \hat{G}_0^S \end{pmatrix} \begin{pmatrix} \hat{V}_1^{PP} & \hat{V}_1^{PS} \\ \hat{V}_1^{SP} & \hat{V}_1^{SS} \end{pmatrix} \begin{pmatrix} \hat{G}_0^P & 0 \\ 0 & \hat{G}_0^S \end{pmatrix} \begin{pmatrix} \hat{V}_1^{PP} & \hat{V}_1^{PS} \\ \hat{V}_1^{SP} & \hat{V}_1^{SS} \end{pmatrix} \begin{pmatrix} \hat{G}_0^P & 0 \\ 0 & \hat{G}_0^S \end{pmatrix} \\ & \vdots \end{aligned}$$

Hence, for $\hat{V}^{PP} = \hat{V}_1^{PP} + \hat{V}_2^{PP} + \hat{V}_3^{PP} + \dots$ any one of

the four matrix elements of V requires $\begin{pmatrix} \hat{D}^{PP} & \hat{D}^{PS} \\ \hat{D}^{SP} & \hat{D}^{SS} \end{pmatrix}$

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- \hat{D}^{PP} can be determined independently
in terms of $\begin{pmatrix} \hat{V}^{PP} & \hat{V}^{PS} \\ \hat{V}^{SP} & \hat{V}^{SS} \end{pmatrix}$
 - but \hat{V}^{PP} or $\hat{V}^{PS}, \hat{V}^{SP}, \hat{V}^{SS}$ requires $\begin{pmatrix} \hat{D}^{PP} & \hat{D}^{PS} \\ \hat{D}^{SP} & \hat{D}^{SS} \end{pmatrix}$
 - That's what the general relationship
 $G = G_0 + G_0 V G$ requires.
 - A direct non-linear solution
order by order in the data matrix $\begin{pmatrix} \hat{D}^{PP} & \hat{D}^{PS} \\ \hat{D}^{SP} & \hat{D}^{SS} \end{pmatrix}$

-
- ISS is not iterative linear inversion.

- Iterative linear starts with $G_0 V_1 G_0 = D$ (7)

solves for V_1 , changes the reference medium, finds a new L_0 and G_0 (and require generalized inversions of noisy bandlimited data dependent operators).

- To find V_1' , $G_0' V_1' G_0' = D' = (G - G_0')_{ms}$

$$L_0' = L_0 - V_1$$

$$L_0' G_0' = \delta$$

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- The problem is much more serious than a different approach to solve $G_0 V_1 G_0 = D$ (7) for V_1 .
 - If (7) is our entire basic theory, you can mistakenly think that $\hat{D}^{PP} = \hat{G}_0^P \hat{V}_1^{PP} \hat{G}_0^P$ is sufficient to update $\hat{D}^{PP'} = \hat{G}_0^{P'} \hat{V}_1^{PP'} \hat{G}_0^{P'}$
 - That step loses contact with and violates

$$G = G_0 + G_0 V G$$

for the elastic wave equation.

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1. That is, it violates the basic relationship between changes in a medium, \mathbf{V} and changes in the wavefield, $\mathbf{G}-\mathbf{G}_0$ for the simplest elastic model.
 2. This direct inverse method gives you a platform for FWI and communicates when a “FWI” method should work in principle.
 3. Iteratively inverting multi-component data has the correct data but doesn't corresponds to a direct inverse algorithm.
 4. To honor $\mathbf{G}=\mathbf{G}_0+\mathbf{G}_0\mathbf{V}\mathbf{G}$, you need both the data and the algorithm that direct inverse prescribes.

A.B. Weglein and Jinlong Yang

A first comparison of the inverse scattering series and iterative linear inverse for parameter estimation, M-OSRP (2015), SEG Abstract (2015).

There's a role for direct and indirect methods in practical real world application.

4D Application

Discrimination between pressure and fluid saturation using direct non-linear inversion method: *an application to time-lapse seismic data*

Haiyan Zhang, Arthur B. Weglein, Robert Keys, Douglas Foster and Simon Shaw

M-OSRP Annual Meeting
University of Houston
May 10 –12, 2006

Statement of the problem

- Distinguishing pressure changes from reservoir fluid changes is difficult with conventional seismic time-lapse attributes.
- Pressure changes or fluid changes?
 - shear modulus *sensitive to* **pressure** changes
 - V_p/V_s *sensitive to* **fluid** changes
- A direct non-linear inversion method may be useful for accomplishing this goal.

Introduction of the method

Inverse scattering series

Time-lapse seismic monitoring

Reference medium L_0	Initial reservoir condition
Actual medium L	Current reservoir condition
Earth property changes in space $V=L_0-L$	Reservoir property changes in time
Reference wave field G_0	Baseline survey
Actual wave field G	Monitor survey
Scattered wave field $D=G-G_0$	Monitor-Baseline

Conclusion

- **Comparing the first and second order algorithms in estimating shear modulus and V_p/V_s contrasts.**
- **Second order direct inverse was able to distinguish pressure changes from fluid changes.**

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Sponsors



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